



Using Advanced Energy Methods to Enhance FEA and Experiments

Ted Diehl, PhD

Kinetic Energy Viscous Dissipation
Potential Energy
Internal Energy
Artificial Energy Frictional Dissipation
Plastic Dissipation
Energy Derivatives



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Overview

- Conservation of energy and the energy balance
 - Typical FEA analyst's use of energy
 - Assessing energy quantities to determine plausibility of FEA
 - Advanced uses of energy and energy methods
 - Using Energy Methods to estimate impact behavior from quasi-static data
 - Nonlinear and linear problems
- ➡
- Causality and Energy Derivatives
 - Using Derivatives of Energy to
 - Correct/adjust models to remove undesirable distortions
 - Create fast predictions from existing data

Several examples demonstrating techniques
that enhance Abaqus FEA and experiments



Conservation of Energy and the Energy Balance

Applied External Work =

Abaqus outputs all these energy quantities, and more, if you ask for it!

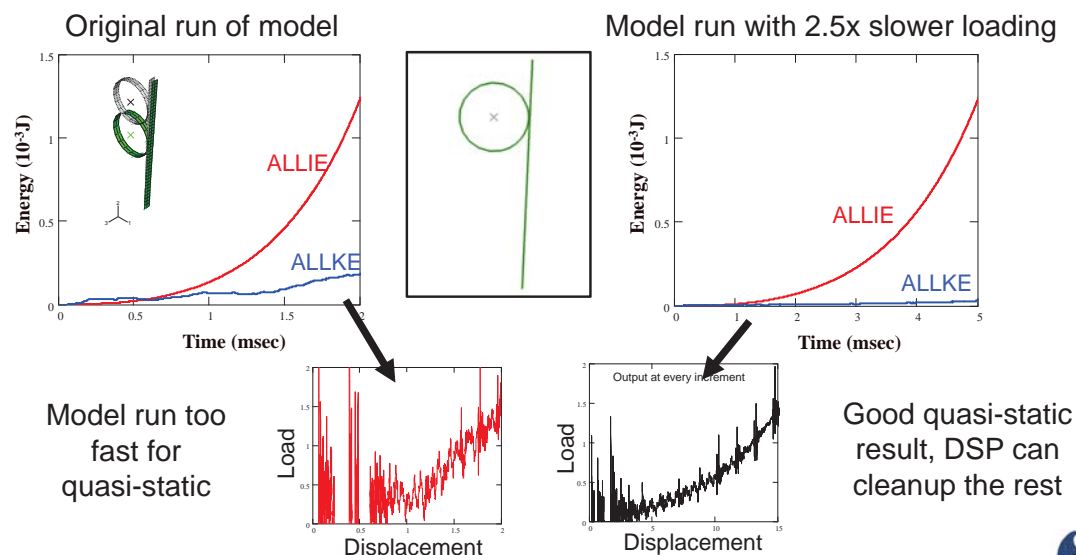
Internal Strain Energy + Kinetic Energy + Dissipation Effects

- $WK + HF = IE + KE + FD + VD + IHE - \text{Other}$
 - $IE = SE + PD + CD + DMD + FC + AE + DC$
- Various energy terms
 - External Work, External Heat Flux, Internal Strain Energy, Kinetic Energy, Frictional Dissipation, Viscous Dissipation, Internal Heating, Energy associated with Penalties and Mass Scaling, Recoverable Strain Energy, Plastic Dissipation, Viscoelasticity, Damage, Fluid Cavity Energy, Artificial Hourglass Control Energy, Distortion Control, and the Kitchen Sink!



Typical Use of Energy Quantities to Assess FEA Plausibility

- Energy plots are helpful in Explicit Dynamics models to determine if Kinetic Energy is significant.
 - This is very helpful when performing quasi-static analysis via Explicit FEA.



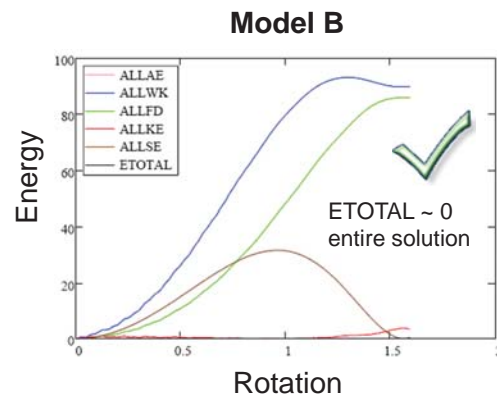
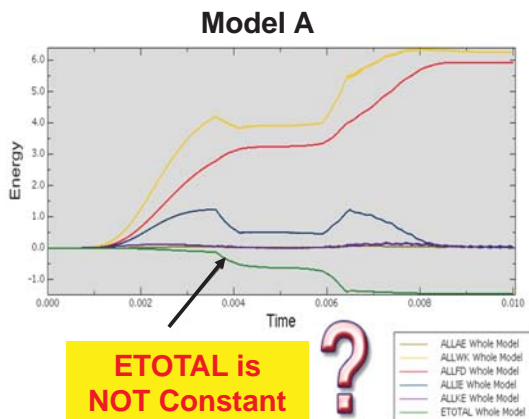
Checking the Energy Balance with ETOTAL

- In Abaqus, the energy balance equation for the entire model is written as
 - $ETOTAL = \sum_{ALL}(-WK - HF + IE + KE + FD + VD + IHE - Other)$
 - Same equation as before, but the work is moved to same side as other quantities and ETOTAL is introduced.
 - ETOTAL is a catch-all quantity.
 - **ETOTAL should remain constant throughout the entire solution.**
 - It is typically zero, or very near zero.
 - Models with initial kinetic energy will have large non-zero ETOTAL, but it should still be constant over the solution duration.



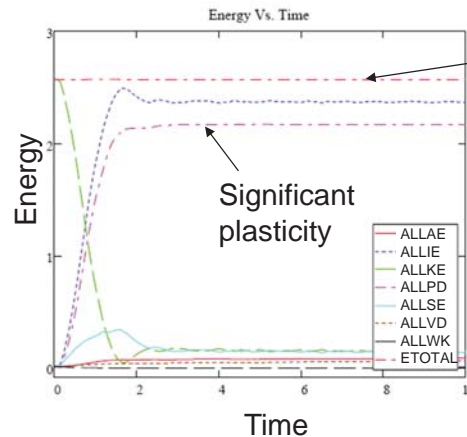
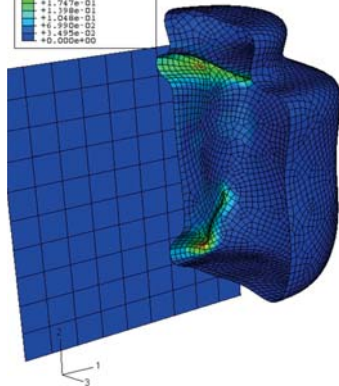
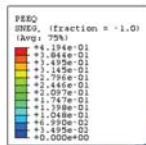
Using an ETOTAL Check to Find a Problem with a Model

- Here are energy assessments from two unrelated models.
 - **Model A** likely has something drastically wrong, as ETOTAL varies significantly relative to other energy terms.
 - **This plot led the analyst to ultimately find a bug in the model.**
 - **Model B** indicates that ETOTAL is constant and thus the results pass this sanity check.



Unfortunately, Energy is NOT in the front of FEA Users Minds

- Most FEA analysts look at deformed shapes, stress and strain contours, displacements and reaction forces.
 - Many less FEA users frequently look at plots of energy**
 - Very few do any additional calculations with energy quantities**



ETOTAL is non-zero, BUT constant. It is non-zero due to large initial kinetic energy in the problem.

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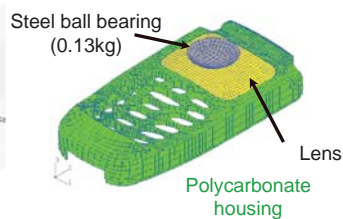
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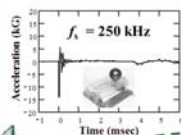
Using Energy Methods to Estimate Impact Behavior from Quasi-Static Data



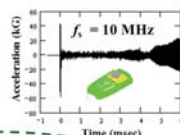
Accelerometer mounted
bottom-side of lens



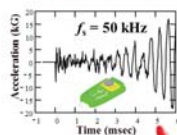
Experimental Data
(Alias Protected)



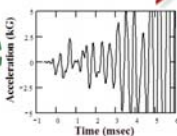
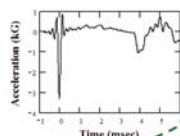
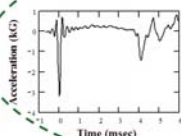
FEA Data
(Alias Protected)



FEA Data
(Unprotected)



After 5 kHz lowpass Butterworth filtering



**Can I do any
useful analysis of
a severe impact
problem like this
without resorting
to a transient
dynamic analysis
???**

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Ref: Diehl, et. al., "Using Digital Signal Processing ...",
Abaqus Users' Conference, Chester, United Kingdom, 1999.

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Energy Methods to Estimate Impact Behavior

• Basic approach and assumptions

- Combine Static Analysis & Energy Methods to predict Impact results.
 - Energy is always conserved (underlying principle).
- **Kinetic Energy** (just before impact) \Rightarrow **(IE + FD)** at “peak event time”
 - IE contains elastic and inelastic energy.
- **Apply Static Load/BCs until $IE + FD = KE$** (prior to impact)
 - Statically deform structure into the expected dynamic deformation.
- The energy transfer assumption is typically a conservative assumption and only good for certain cases.
 - In a general drop problem, the structure will always have a mix of kinetic and stored internal energy throughout the impact event.
- Considers only “1st mode deformation”.
 - Higher modes are ignored.
- Material strain rate sensitivity is ignored.
 - Use properties “at rate” in quasi-static simulation (not possible in physical test)



Energy Methods to Estimate Impact Behavior

• Additional comments

- Must define sufficient static displacement B.C.'s to avoid rigid body motion.
 - Consider the use of Inertial Relief in certain simulations to avoid over constraining with displacement BCs.
- Understanding what is the correct static deformation mode to apply is not too difficult in some cases & nearly impossible in other cases.

• Accuracy

- Most accurate for Displacement results.
- Stress and Strain are reasonably accurate.
- Acceleration not computed in a static model.
- Strain-Rate Dependence of Material Behavior is Ignored.
 - May be significant in plastics and polymers!

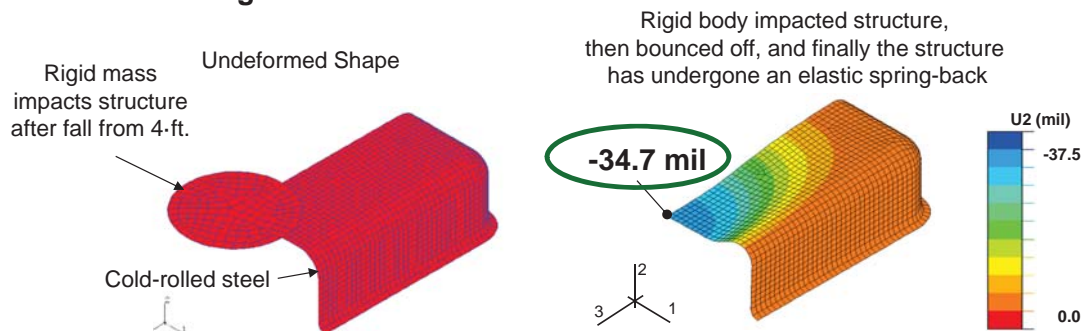
Remember, this is only an approximation and the underlying assumptions must be valid.



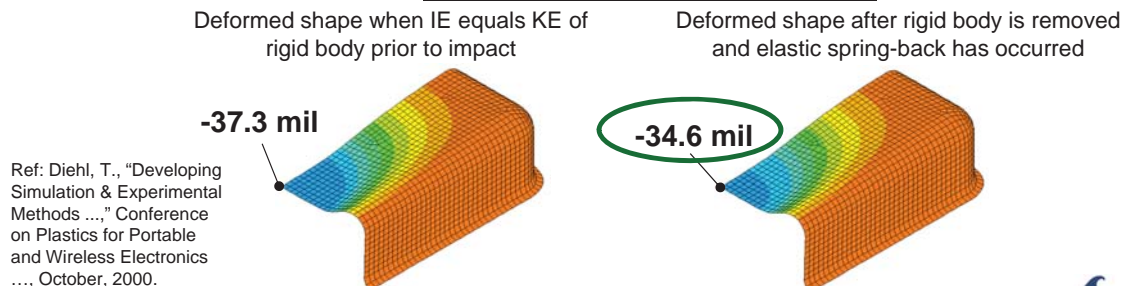
Energy Methods to Estimate Impact Behavior

• Steel Shell Denting

Explicit Dynamics Model That Includes Plasticity



Static Model That Includes Plasticity



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Energy Methods to Estimate Impact Behavior

• Phone drop problem

- Design a physical test to determine if the antenna support will compress enough to have the antenna leg deform too far into the phone housing, causing a chip on the circuit board to be broken off?

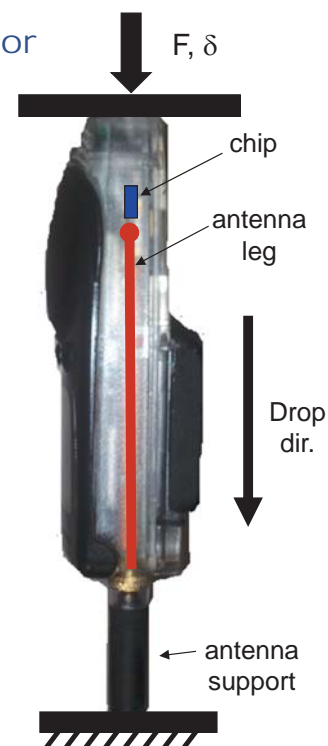
- Phone is dropped from 2-m

• Solution

- Assume that housing stiffness is much larger than antenna support and chip/board stiffness
- Compress phone in Instron (or MTS) uniaxial tester.
- Record load and cross-head displacement
 - Integrate to get applied work vs displacement
- Stop test when work equals mgh
 - $M = \text{mass of phone}$, $g = 9.81 \cdot \text{m/s}^2$, $h = 2 \cdot \text{m}$

Ref: Diehl, T., "Developing Simulation & Experimental Methods ...,"
Conf. on Plastics for Portable and Wireless Electronics ..., October, 2000.

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Simple Scaling Equation to Estimate Impact Behavior for Problems with Linear Response

- Linear Structure - No plasticity or changing contact.

$$F = Ku \quad SE = \frac{1}{2} Ku^2 \quad W = \int_0^x F(u) du = \frac{1}{2} Fx$$

- Energy from Dynamics (Potential Energy & Kinetic Energy)

$$PE = mGh \quad KE = \frac{1}{2} mv^2 \quad m = \text{mass}, h = \text{drop height}, v = \text{velocity}$$

- These energies determine **DEPTI** (Dynamic Energy Prior To Impact).
- Scale any static response from model, r_{static} , to get dynamic response, r_{dyn} , by

$$r_{dyn} = r_{static} \sqrt{\frac{DEPTI}{SE + FD}}$$

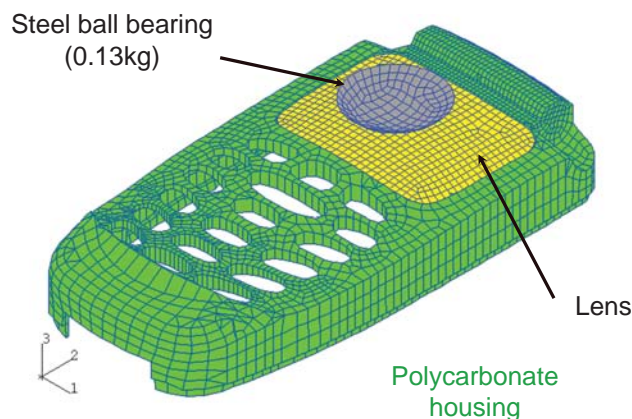
Structure is statically deformed into expected "impact deformation mode"



Simple Scaling Equation to Estimate Impact Behavior for Problems with Linear Response

- Lens Impact Analysis**

- Steel ball bearing dropped 0.5m



$$r_{dyn} = r_{static} \sqrt{\frac{DEPTI}{SE + FD}}$$

Max Lens Displacement

Estimate via Statics + Energy Meth.	Actual Impact Simulation
3.68mm	3.76mm

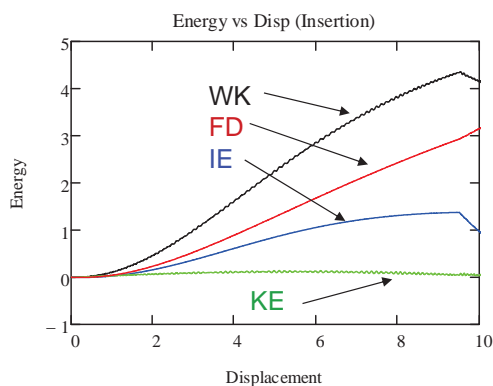
Scaled static estimate accuracy 0.979

Quasi-static solution derived from model published in the following paper:
Diehl, et. al., "Using Digital Signal Processing ...",
Abaqus Users' Conference, Chester, United Kingdom, 1999.

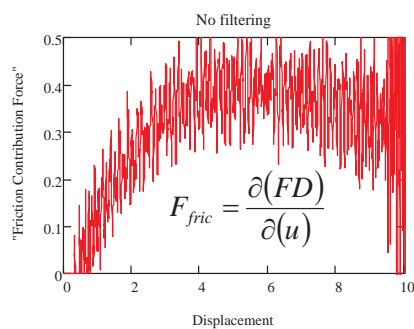
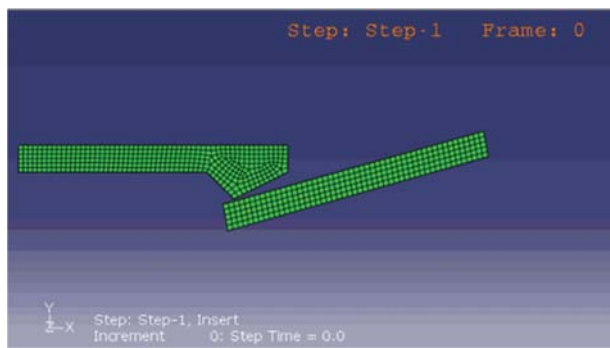


Causality and Energy Derivatives

- Can Energy tell me what's the largest **Cause** of the force I feel when I load a structure?
 - Corollary – What materials, components, etc. have little influence on performance?



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Causality and Energy Derivatives

- Basic relationships
 - External Work

$$W = \int F du$$

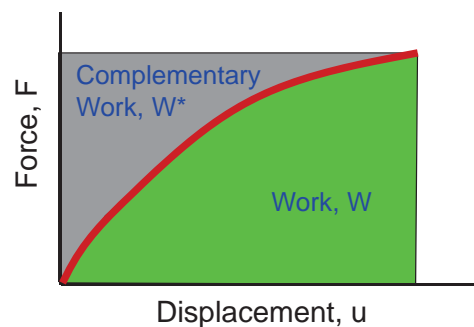
- External Complementary Work

$$W^* = \int u dF$$

- Observations

- $$\frac{\partial(WK)}{\partial(u)} = F_{applied}$$
- Derivatives of external complementary work with respect to forces produce displacements or displacement-like quantities.
 - Derivative with respect to rotation produce moments.

Measures of work from applied loads and displacements



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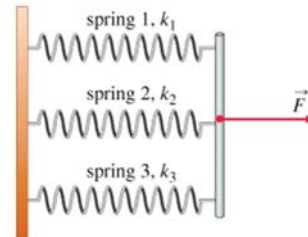
Causality and Energy Derivatives

- Simplified Energy Balance (ignoring some terms)
 - **WK = IE + KE + FD**
- Derivatives of energy relate directly to the force balance for springs in parallel

$$\frac{\partial(WK)}{\partial(u)} = F_{\text{applied}} = \frac{\partial(IE)}{\partial(u)} + \frac{\partial(KE)}{\partial(u)} + \frac{\partial(FD)}{\partial(u)} = \Phi_{IE} + \Phi_{KE} + \Phi_{FD}$$

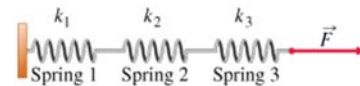
• Springs in Parallel

- Force balance: $F_{\text{total}} = F_1 + F_2 + \dots$
- Displacements: $\Delta L_{\text{total}} = \Delta L_1 = \Delta L_2 = \dots$



• Springs in Series

- Force balance: $F_{\text{total}} = F_1 = F_2 = \dots$
- Displacements: $\Delta L_{\text{total}} = \Delta L_1 + \Delta L_2 + \dots$



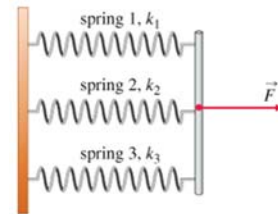
Need force derivatives of Complementary Work



Causality and Energy Derivatives

- Simplified Energy Balance (ignoring some terms)
 - **WK = IE + KE + FD**
- Derivatives of energy relate directly to the force balance for springs in parallel

$$\frac{\partial(WK)}{\partial(u)} = F_{\text{applied}} = \frac{\partial(IE)}{\partial(u)} + \frac{\partial(KE)}{\partial(u)} + \frac{\partial(FD)}{\partial(u)} = \Phi_{IE} + \Phi_{KE} + \Phi_{FD}$$



• Causality Coefficients $\Rightarrow \Phi_{IE}, \Phi_{KE}, \Phi_{FD}$

- Terms assess contributions to overall structural response.
- Use to determine what to change to have most influence on response.
 - Can be grouped by part, material, element set, ...
- Can make estimated prediction equations for changes in quantities without the need to run the entire model again (or run a physical test again)!



Causality and Energy Derivatives – Creating a “Hit List”

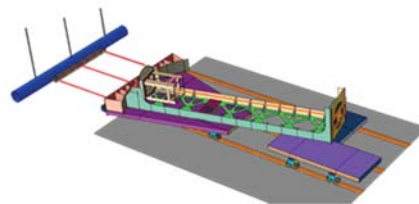
- Given a structure with a variety of components and materials, how can a “Hit List” of best candidates for modification be created to increase (or decrease) overall structure stiffness?
 - Can this be done with single simulation run?
 - Will it work for nonlinear problems too?

- Answer – YES**

- Via Causality and Energy Derivatives**

- Analyze model for a specified set of BC's and loads (linear or nonlinear).
 - Output IE (and other energies) grouped by component, material ...
 - Derivatives of energy relative to applied BC displacement

- ⇒ **Causality Coefficients**



WOX Shock Tester with permission from Jon Yaglia, Naval Surface Warfare Center, Dahlgren Div.



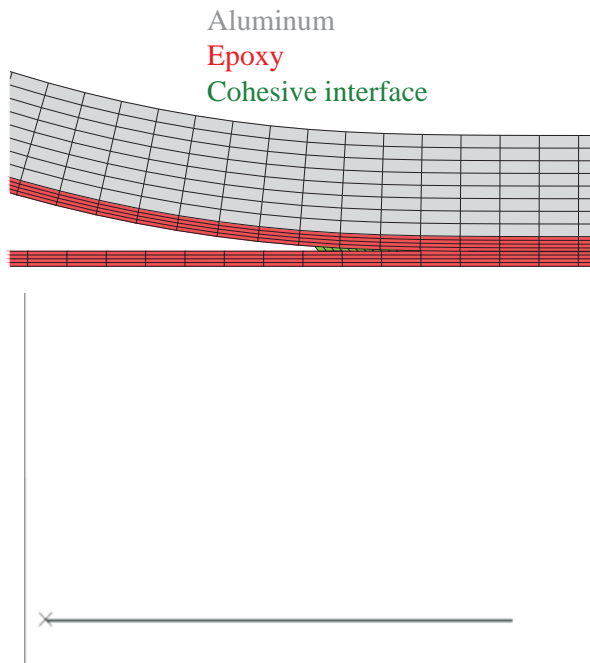
Causality and Energy Derivatives

$$\frac{\partial(WK)}{\partial(u)} = F_{\text{applied}} = \frac{\partial(IE)}{\partial(u)} + \frac{\partial(KE)}{\partial(u)} + \frac{\partial(FD)}{\partial(u)} = \Phi_{IE} + \Phi_{KE} + \Phi_{FD}$$

- Estimating changes in a structures response from energy derivatives
 - Derivatives of **IE** ⇒ how component stiffness changes affect response.
 - Stiffness changes including changes in material or geometry.
 - Derivatives of **KE** ⇒ how kinetic energy (mass or velocity) changes affect response.
 - Derivatives of **FD** ⇒ how coefficient of friction changes affect response.
- These estimates of change or influence are most accurate if the structure's components behave as springs in parallel.
 - Assessing energy derivatives for structures with components that act like springs in series is also helpful, but more difficult and typically less accurate since obtaining complimentary energy is often impossible and must be estimated.



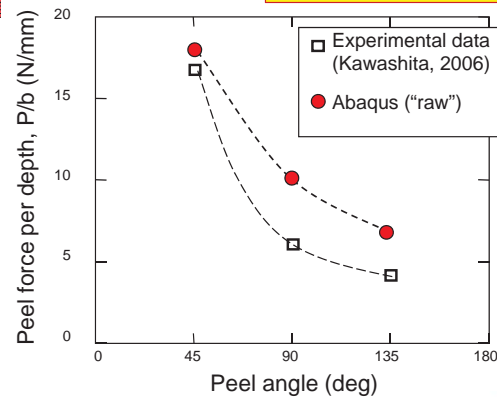
FE Modeling of Peeling Via Cohesive Elements



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- Abaqus/Explicit model
 - Plasticity plus cohesive elems.
 - Adaptive mass scaling of cohesive elements
 - Solution/experiment correlation is "so so"

Hey, Peeling is a Tough Problem

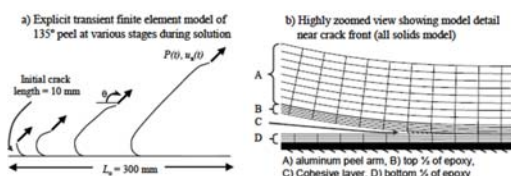


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FE Modeling of Peeling Via Cohesive Elements

Improving Quasi-Static Estimate



Adjusting the Peel force by removing the force associated with the kinetic energy

$$P_{KE} = \frac{d}{dx} \left(\frac{d}{dt} \left(\frac{1}{2} \frac{ALLKE}{\dot{u}x} \right) \right) = \frac{ALLKE}{\dot{u}x}$$

Computing numerical derivatives

$$ALLKE_i := \text{derivative}_k(t_i, ALLKE_i, \dots) \quad \dot{u}x_i := \text{derivative}_k(t_i, \dot{u}x_i, \dots)$$

$$P_{KE_i} := \frac{ALLKE_i}{\dot{u}x_i} \quad \text{Calculation of quasi-static peel force without kinetic energy contributions} \quad \Rightarrow \quad P_{qs_i} := P_{total_i} - P_{KE_i}$$

Specify a case to plot $num := 63$ $cases_{num} := "case_22g_135deg_1p32G"$

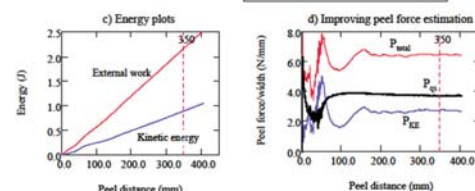
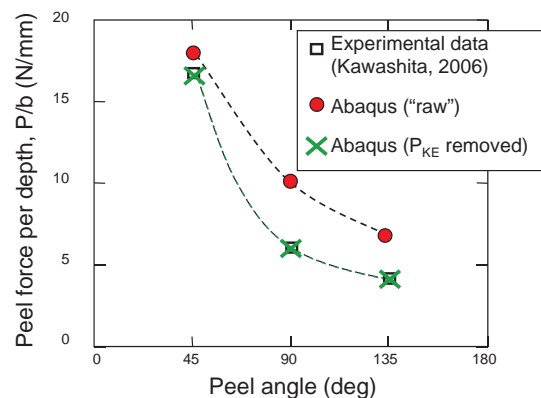


Figure 6: Significantly enhancing analysis accuracy and solution speed by adjusting the calculated peel load using derivatives of computed energy terms.

In this example, correcting for so-called "kinetic energy force" in quasi-static explicit FEA model makes significant improvement!



Ref:

Diehl, T., "Integrating Theory, Experiments, and FEA to Solve Challenging Nonlinear Mechanics Problems," *Abaqus Users' Conference Proceedings*, 2008.

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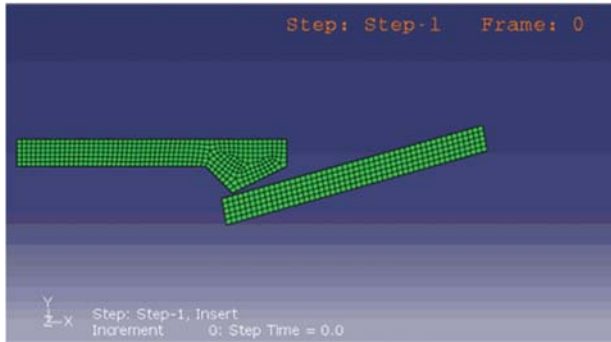
Quasi-Static Snap-Fit Via Explicit Dynamics FEA

Preliminary scouting analysis of a Snap-Fit design

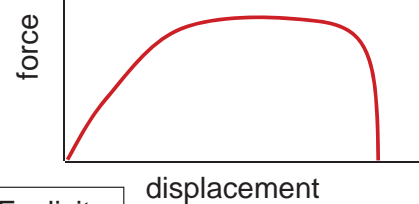
- Understand sensitivity to lower arm angle and influence of friction.
- Simulate both insertion and retraction
 - Implicit FEA will have difficulty with “snap” and retraction, so simulate with Explicit FEA.



3 angles: θ_o , θ_o+5° , θ_o-5°



“Form” of expected physical response during insertion



FEA via Abaqus/Explicit,
Filtering via Kornucopia®

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Quasi-Static Snap-Fit Via Explicit Dynamics FEA Insertion Results Using Different Output Requests



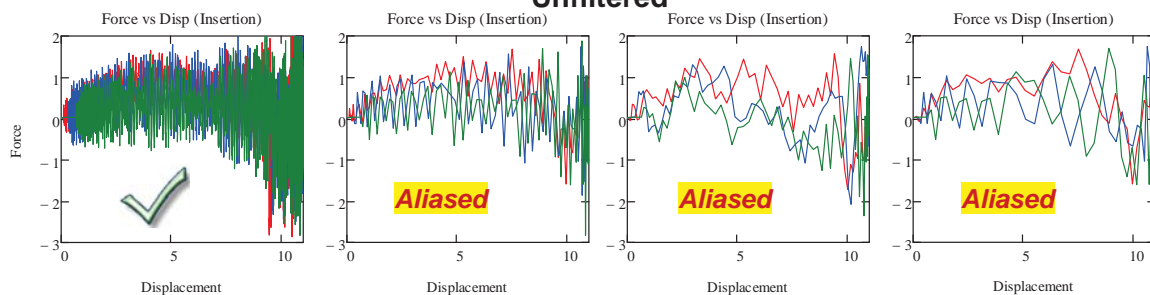
Every increment
(~35,000 incs)

100 increments

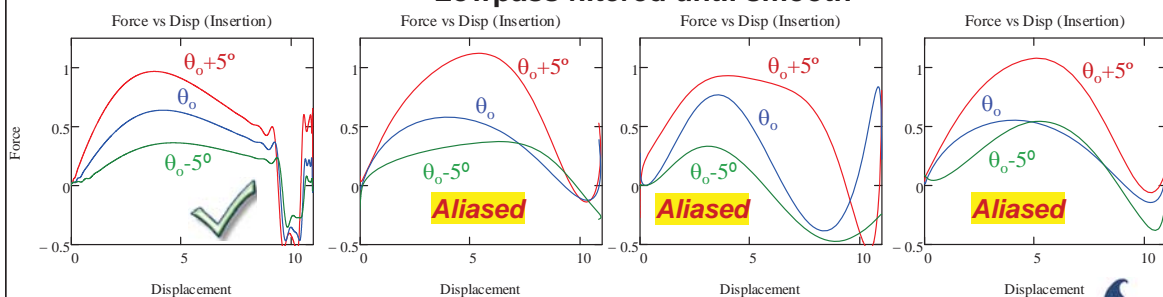
80 increments

50 increments

Unfiltered



Lowpass filtered until smooth

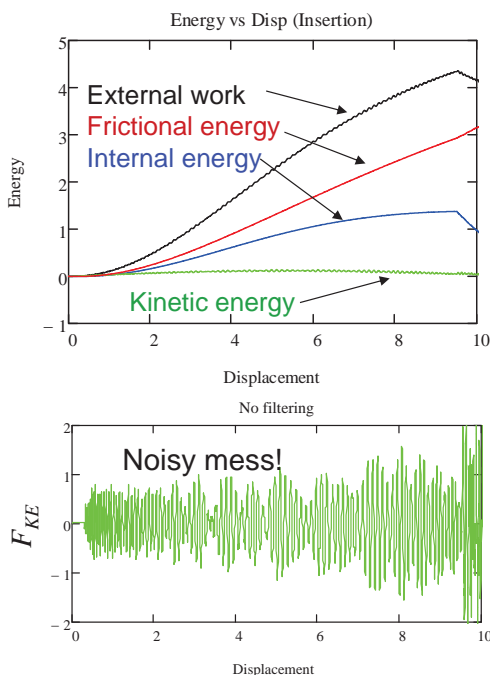


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Quasi-Static Snap-Fit Via Explicit Dynamics FEA Energy Methods, Derivatives, and DSP to Improve Analysis



Below are two “forces” derived from derivatives of energy quantities. In certain cases, such quantities can be used to enhance results interpretations.

Kinetic Force – load associated with moving mass.

$$F_{KE} = \frac{\partial(U_{KE})}{\partial(u)}$$

U_{KE} – kinetic energy
 u – displacement

Frictional Force – portion of total load caused by friction.

$$F_{fric} = \frac{\partial(U_{friction})}{\partial(u)}$$

$U_{friction}$ – total energy consumed by friction

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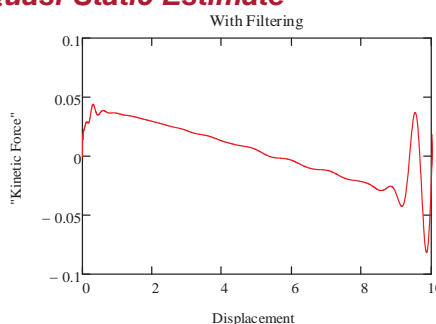
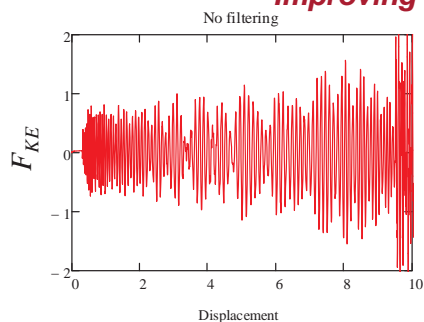
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Quasi-Static Snap-Fit Via Explicit Dynamics FEA Energy Methods, Derivatives, and DSP to Improve Analysis

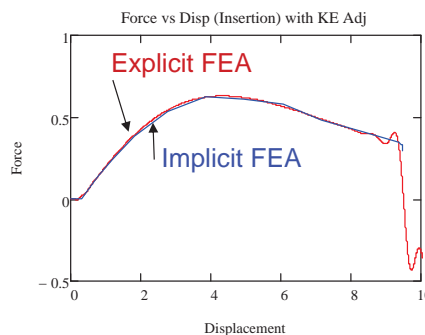
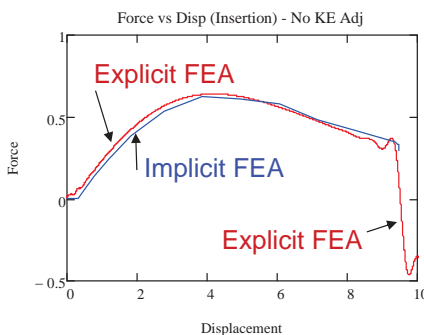


Improving Quasi-Static Estimate



Case: θ_0

Filtered via
bi-directional lowpass
6th order butterworth,
 $f_c = 0.005 \cdot f_s$



The small difference between the implicit FEA and explicit FEA results is shown to be a result of “moving mass”.

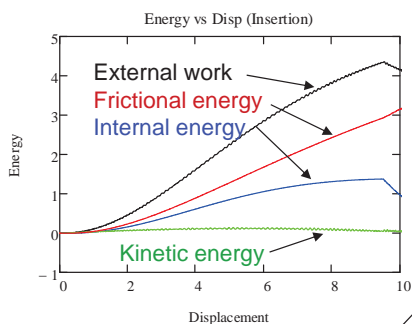
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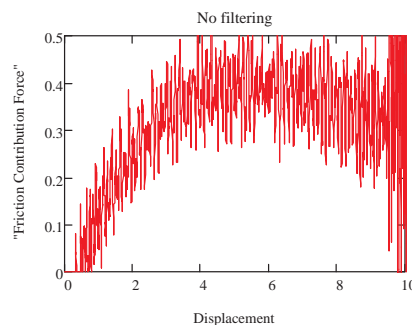
Quasi-Static Snap-Fit Via Explicit Dynamics FEA Energy Methods, Derivatives, and DSP to Improve Analysis

Estimating Frictional Influence

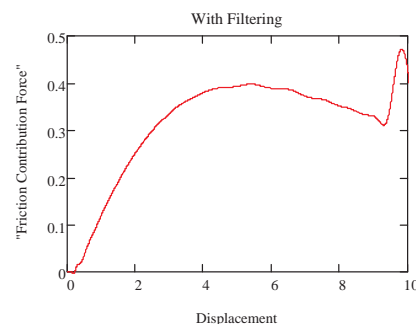


$$F_{fric} = \frac{\partial(U_{friction})}{\partial(u)}$$

Similar computations for
 $\theta_0 + 5^\circ$ and $\theta_0 - 5^\circ$



Case: θ_0

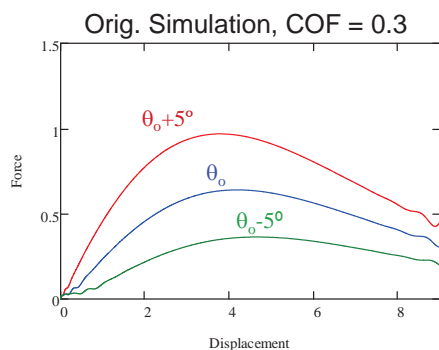


Filtered via
bi-directional lowpass
6th order butterworth,
 $f_c = 0.005 \cdot f_s$



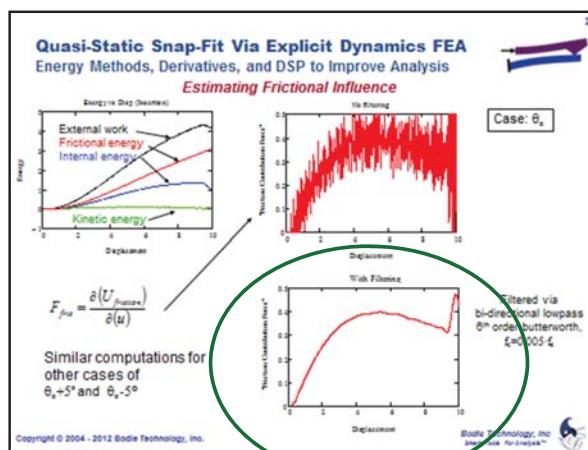
Quasi-Static Snap-Fit Via Explicit Dynamics FEA Energy Methods, Derivatives, and DSP to Improve Analysis

Estimating Frictional Influence



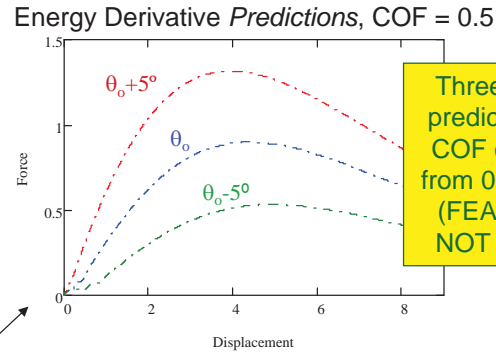
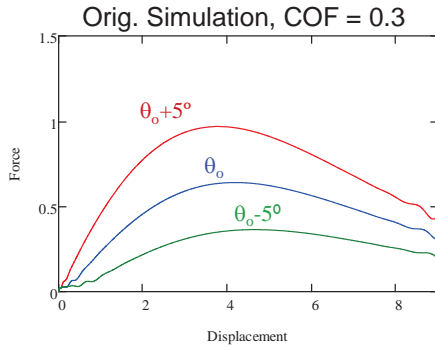
Prediction equation

$$F_{total}|_{COF=new} = F_{total}|_{COF=0.3} + F_{fric}|_{COF=0.3} \cdot \left(\frac{COF_{new}}{COF=0.3} - 1 \right)$$



Quasi-Static Snap-Fit Via Explicit Dynamics FEA Energy Methods, Derivatives, and DSP to Improve Analysis

Estimating Frictional Influence

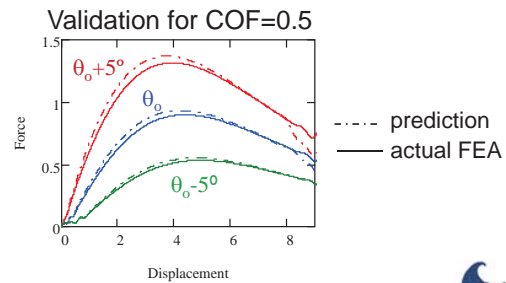


Three FAST predictions of COF change from 0.3 to 0.5 (FEA model NOT re-run)

Prediction equation

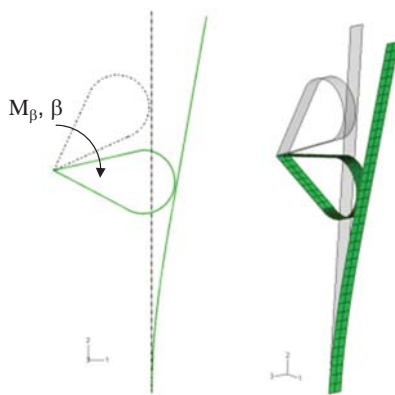
$$F_{total|COF=new} = F_{total|COF=0.3} + F_{fric|COF=0.3} \cdot \left(\frac{COF_{new}}{COF=0.3} - 1 \right)$$

Validating predictions by running actual full FEA models for all three angle cases with COF = 0.5

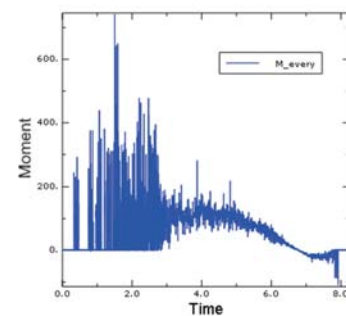
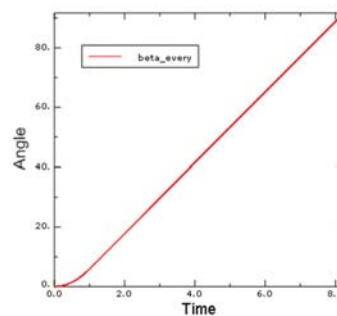
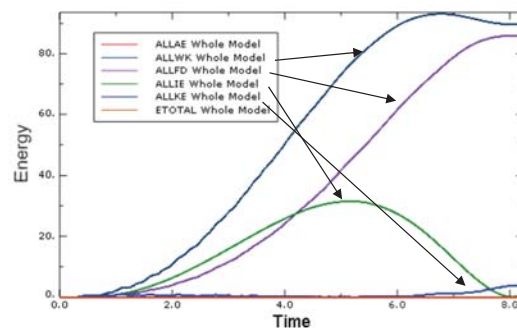


Getting More Out of Models

- Starting with this:
 - Running model only **ONCE**.

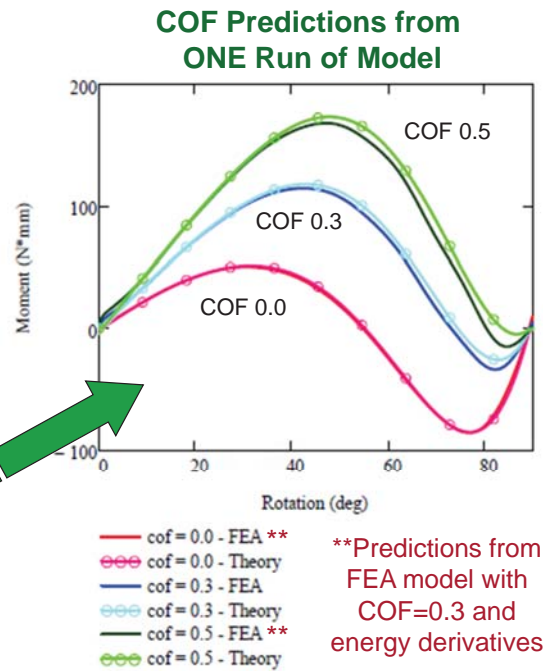
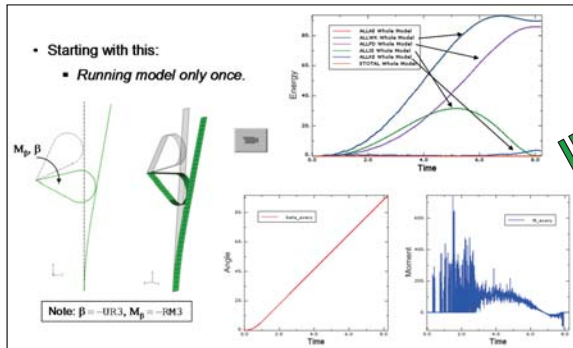


Note: $\beta = -UR3$, $M_\beta = -RM3$



Getting More Out of Models

- We get these results by use of DSP and Energy Derivatives!
 - Accurate results that match benchmark
 - Prediction of friction influence WITHOUT additional runs of model!**



Conclusions

- Energy Balance MUST be satisfied
 - Confirming $ETOTAL = Constant$ is a key sanity check for ALL models
- Assessing Kinetic Energy relative to Work and IE is important for Quasi-static Explicit Dynamics models
- Many engineers doing FEA and/or physical testing underutilize Energy Methods
- Energy Methods can be effectively used to estimate impact behavior with Quasi-static models or experiments.
 - Powerful technique, but limitations apply (read fine print!)
- Causality is derived from energy derivatives
 - Most accurate for structures with behavior similar to springs in parallel
 - Enables computing "Hit List" of key components/materials from single run
 - Enables fast prediction equations (good for linear and nonlinear problems)

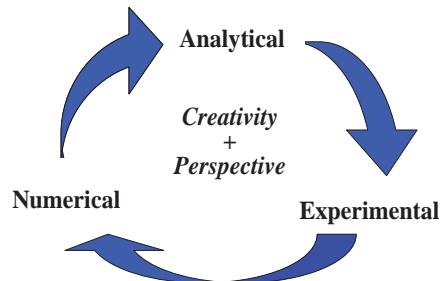


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 - Led nonlinear mechanics efforts at Kodak, Motorola, and DuPont
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 - Cell-phone impact
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 - Paper motion in copiers
 - Simulating fabrics
 - Flexible structures
 - Nonlinear nip mechanics
 - Ballistic protection
 - Nonlinear materials
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